



EXPERIMENTAL EVIDENCE FOR VIBRATIONAL RESONANCE AND ENHANCED SIGNAL TRANSMISSION IN CHUA'S CIRCUIT

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We consider a single Chua's circuit and a system of a unidirectionally coupled n -Chua's circuits driven by a biharmonic signal with two widely different frequencies ω and Ω , where $\Omega \gg \omega$. We show experimental evidence for vibrational resonance in the single Chua's circuit and undamped signal propagation of a low-frequency signal in the system of n -coupled Chua's circuits where only the first circuit is driven by the biharmonic signal. In the single circuit, we illustrate the mechanism of vibrational resonance and the influence of the biharmonic signal parameters on the resonance. In the $n(=75)$ -coupled Chua's circuits enhanced propagation of low-frequency signal is found to occur for a wide range of values of the amplitude of the high-frequency input signal and coupling parameter. The response amplitude of the i th circuit increases with i and attains a saturation. Moreover, the unidirectional coupling is found to act as a low-pass filter.

Keywords: Chua's circuit; unidirectionally coupled Chua's circuits; vibrational resonance; enhanced signal propagation.

1. Introduction

A nonlinear system driven by a biharmonic force with two widely different frequencies say, ω and Ω with $\Omega \gg \omega$, can exhibit resonance at the low-frequency ω when the amplitude g or frequency Ω of the high-frequency component is varied. This

high-frequency driving force induced resonance is termed as vibrational resonance [Landa & McClintock, 2000; Blekhman & Landa, 2004]. This phenomenon can be used to identify a weak signal as well as to enhance the response of a system. Vibrational resonance has been analyzed in different

kinds of systems such as monostable [Jeyakumari *et al.*, 2009], bistable [Landa & McClintock, 2000; Gitterman, 2001; Baltanás *et al.*, 2003; Blekhman & Landa, 2004; Chizhevsky, 2008], multistable [Rajasekar *et al.*, 2011], excitable [Ullner *et al.*, 2003] and time-delayed [Yang & Liu, 2010; Jeevarathinam *et al.*, 2011; Daza *et al.*, 2013] systems. Experimental evidence of vibrational resonance in an analog circuit simulation of an excitable system [Baltanás *et al.*, 2003] and in a vertical cavity surface emitting laser system [Chizhevsky & Giacomelli, 2006, 2008] have been reported. Recently, its occurrence is studied in nonlinear maps [Rajasekar *et al.*, 2012], small-world networks [Deng *et al.*, 2010; Yu *et al.*, 2011] and in coupled oscillators [Yao & Zhan, 2010].

Study of a nonlinear phenomenon in a variety of dynamical systems help us to deeply understand its various features and also explore its applicability in real practical situations. In this connection we wish to point out that an analysis of the different phenomena occurring in nonlinear electronic circuits is of great significance. In nonlinear circuit analysis, Chua's circuit is commonly used as a prototype circuit to investigate a variety of dynamics. Though the recent analysis on Chua's circuit and its variant circuits like the modified Chua's circuits, etc., is exhaustive, we mention some of the noteworthy analysis. Experimental study of jump resonance [Buscarino *et al.*, 2009], infinite cascades of spirals and hubs [Ramirez-Avila & Gallas, 2010], onset of Shilnikov chaos through mixed mode oscillations [Chakraborty & Dana, 2010], amplitude death due to bidirectional coupling of conjugate variables [Singla *et al.*, 2011] and ghost resonance [Gomes *et al.*, 2012] have been reported. Dynamical behavior and stability analysis of the memristor based fractional-order Chua's circuit [Petras, 2010], stability relation of synchronization in a network of Chua's circuits with time-varying coupling [Bhowmick *et al.*, 2012] and features of total sliding-mode control strategy leading to dynamics insensitive to variations in parameters and external disturbance [Wai *et al.*, 2011] are investigated. Applicability of a graph-theoretical approach on synchronization [Chen & Duan, 2008], adaptive synchronization developed for a general class of chaotic systems with unknown time-varying parameters and external perturbations [Koofigar *et al.*, 2011] and the chaotic synchronization for data

assimilation [Nurujjaman *et al.*, 2012] have also been analyzed in coupled Chua's circuits.

The effect of biharmonic force, particularly, the phenomenon of vibrational resonance has not yet been studied experimentally in the Chua's circuit. This is the goal of the present work. Specifically, we consider both a single Chua's circuit and a system of n -coupled Chua's circuits. We focus our interest on the experimental study of vibrational resonance in a single Chua's circuit and in a PSpice (Personal Simulation Program with Integrated Circuit Emphasis) circuit simulation of n -coupled Chua's circuits. Constructing a large size circuit on a circuit board and analyzing its performance have limitations due to the physical effects such as parasitic capacitance effects, internal noise, and mismatch in the circuit components. Further, the tolerance effects and circuit loading can also affect the behavior of the circuit. Moreover, parametric identification during the initial stage of circuit design is difficult because for each parametric values one has to make a search of availability of the off-shelf components. In recent years, circuit simulators based on SPICE, for example PSpice, have been widely used for investigating the dynamics of circuits [Tuinenga, 1995; Roberts & Sedra, 1995; Ozden *et al.*, 2004; Breen *et al.*, 2011; Heo *et al.*, 2012; Zhou & Song, 2012]. Evaluation of circuit functions and performance through PSpice is more productive than on a breadboard. With PSpice one can quickly check a circuit idea and perform simulated test measurements and analysis which are difficult, inconvenient and unwise for the circuits built on a breadboard. Therefore, we preferred PSpice circuit simulation of a system of n -coupled Chua's circuits instead of its real hardware construction.

The single circuit system is driven by the periodic force $f \sin \omega t$ and $g \sin \Omega t$. The response of the circuit displays resonance when the parameter g or Ω of the high-frequency force is varied. To characterize the vibrational resonance, we use the response amplitude Q , the ratio of amplitude A_ω of the output signal at the frequency ω of the input signal and the amplitude f of the input periodic signal $f \sin \omega t$. A_ω can be measured from the power spectrum of the output of the circuit. The signature of the resonance is clearly seen in the quantity Q and time series plot. We are able to identify the influences of the parameters ω , Ω and f on the vibrational resonance. The critical value of g at which the resonance

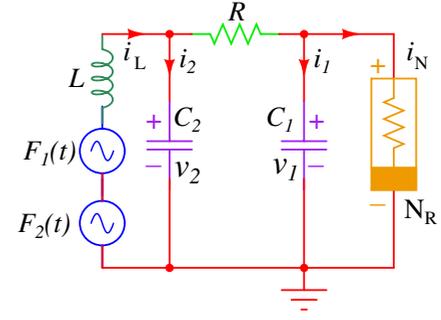
occurs increases linearly with the frequency Ω while the response amplitude at resonance decreases linearly with Ω . In the case of a system of n -coupled Chua's circuits the coupling is unidirectional and only the first circuit is driven by the biharmonic force. The response amplitude Q_i of the i th circuit either increases or decreases with i depending upon the values of the control parameters and approaches a limiting value for large values of i . For a range of values of g and the coupling constant (resistivity of the coupling resistor), an undamped signal propagation with the limiting value of $Q > Q_i$ is achieved. In this case for distant circuits the high-frequency component of the output signal is suppressed and the output signal becomes a rectangular pulse-like form.

2. Single Chua's Circuit

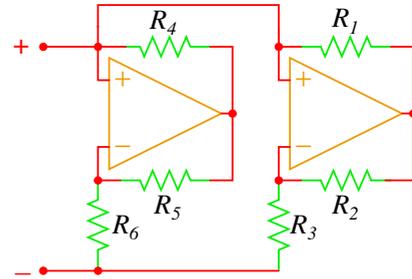
In order to investigate the vibrational resonance, we drive the circuit by a biharmonic force of the form $F(t) = F_1(t) + F_2(t) = f \sin \omega t + g \sin \Omega t$ with $\Omega \gg \omega$. Figure 1(a) depicts the resultant Chua's circuit. The practical realization of the Chua's diode N_R is shown in Fig. 1(b). N_R consists of two operational amplifiers and six linear resistors. The typical voltage-current characteristic of the Chua's diode is shown in Fig. 1(c). It has five-segment piecewise-linear form. Throughout our study we fix the values of the circuit parameters as $C_1 = 10$ nF, $C_2 = 100.5$ nF, $L = 18.75$ mH, $R = 1.98$ k Ω , $R_1 = 222.2$ Ω , $R_2 = 224$ Ω , $R_3 = 2.166$ k Ω , $R_4 = 21.63$ k Ω , $R_5 = 21.79$ k Ω and $R_6 = 3.212$ k Ω . The values of the slopes in the voltage-current characteristic curve of the Chua's diode are $G_a = -0.779$ mA/V, $G_b = -0.4192$ mA/V and $G_c = 4.464$ mA/V, while the values of the break points are $BP_1 = \pm 1.3489$ V and $BP_2 = \pm 9.516$ V. In the absence of a biharmonic force, Chua's circuit for the chosen parametric values has two stable equilibrium points $X_+ = (v_1, v_2, i_L) = (5.656$ V, 0 V, -2.855 mA) and $X_- = (-5.656$ V, 0 V, 2.855 mA) and one unstable equilibrium point $X_0 = (0, 0, 0)$.

By applying Kirchhoff's laws to the various branches of circuit shown in Fig. 1, we obtain the state equations as [Lakshmanan & Murali, 1996; Chen & Ueta, 2002; Fortuna *et al.*, 2009]

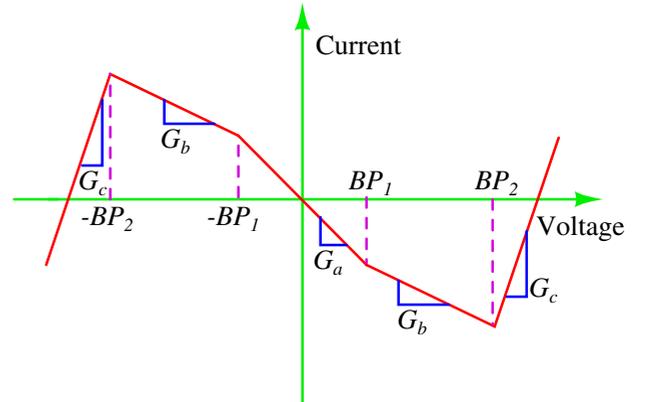
$$C_1 \frac{dv_1}{dt} = \left(\frac{1}{R} \right) (v_2 - v_1) - f(v_1), \quad (1a)$$



(a)



(b)



(c)

Fig. 1. (a) Chua's circuit driven by two periodic forces, $F_1(t) = f \sin \omega t$ and $F_2(t) = g \sin \Omega t$. N_R represents Chua's diode, the nonlinear element of the circuit, (b) schematic diagram of Chua's diode. Here $R_1 = 222.2$ Ω , $R_2 = 224$ Ω , $R_3 = 2.166$ k Ω , $R_4 = 21.63$ k Ω , $R_5 = 21.79$ k Ω and $R_6 = 3.212$ k Ω and (c) the typical characteristic curve of Chua's diode of (b).

$$C_2 \frac{dv_2}{dt} = \left(\frac{1}{R} \right) (v_1 - v_2 + i_L), \quad (1b)$$

$$L \frac{di_L}{dt} = -v_2 + f \sin \omega t + g \sin \Omega t, \quad (1c)$$

where $f(v_1)$ is the mathematical representation of Chua's diode characteristic curve: $f(v_1) = G_b v_1 + 0.5(G_a - G_b)[|v_1 + BP_1| - |v_1 - BP_1|]$. The

dimensionless form of Eq. (1) are

$$\dot{x} = \alpha(y - x - f(x)), \quad (2a)$$

$$\dot{y} = x - y + z, \quad (2b)$$

$$\dot{z} = \beta(-y + f' \sin \omega' \tau + g' \sin \Omega' \tau), \quad (2c)$$

where $f(x) = bx + 0.5(a - b)[|x + 1| - |x - 1|]$, and $v_1 = xBP_1$, $v_2 = yBP_1$, $i_L = BP_1Gz$, $t = C_2\tau/G$, $G = 1/R$, $a = RG_a$, $b = RG_b$, $\alpha = C_2/C_1$, $\beta = C_2R^2/L$, $f = f'BP_1$, $g = g'BP_1$, $\omega = \omega'C_2/G$ and $\Omega = \Omega'C_2/G$.

In the experiment we consider that $\Omega \gg \omega$. Because the driving input signal has two widely different frequencies ω (low-frequency) and Ω (high-frequency) the output signal of the circuit has components at these two frequencies and their linear combinations. Assume that in the absence of high-frequency input signal $g \sin \Omega t$, the amplitude A_ω of the output signal at the low-frequency ω is weak. We are interested in enhancing the amplitude A_ω of the output signal at the frequency ω by the high-frequency input signal $g \sin \Omega t$. To measure

A_ω we consider the fast Fourier transform (FFT) of the output signal obtained using the Agilent (MSO6014A) Mixed Signal Oscilloscope. A small fluctuation of A_ω is observed in the FFT displayed in the instrument. In view of this for better accuracy an average value of A_ω over 25 measurements is obtained. The value of A_ω measured in the FFT is in dBV. It is then converted into the units of V. Then we compute $Q = A_\omega$ (in V)/ f and is termed as the response amplitude of the circuit at the frequency ω [Landa & McClintock, 2000; Blekhman & Landa, 2004].

We fix $f = 0.3$ V, $\omega = 50$ Hz and $\Omega = 500$ Hz. Figure 2 displays the power spectrum of the voltage v_1 of the circuit for four fixed values of the amplitude g of the high-frequency input signal. The amplitude A_ω at $\omega = 50$ Hz increases and then decreases which is a typical signature of resonance. To characterize the resonance we compute Q at the frequencies ω and Ω of voltages v_1 and v_2 and the current i_L for a range of values of the control parameter g . Figure 3(a) shows the variation of Q of v_1

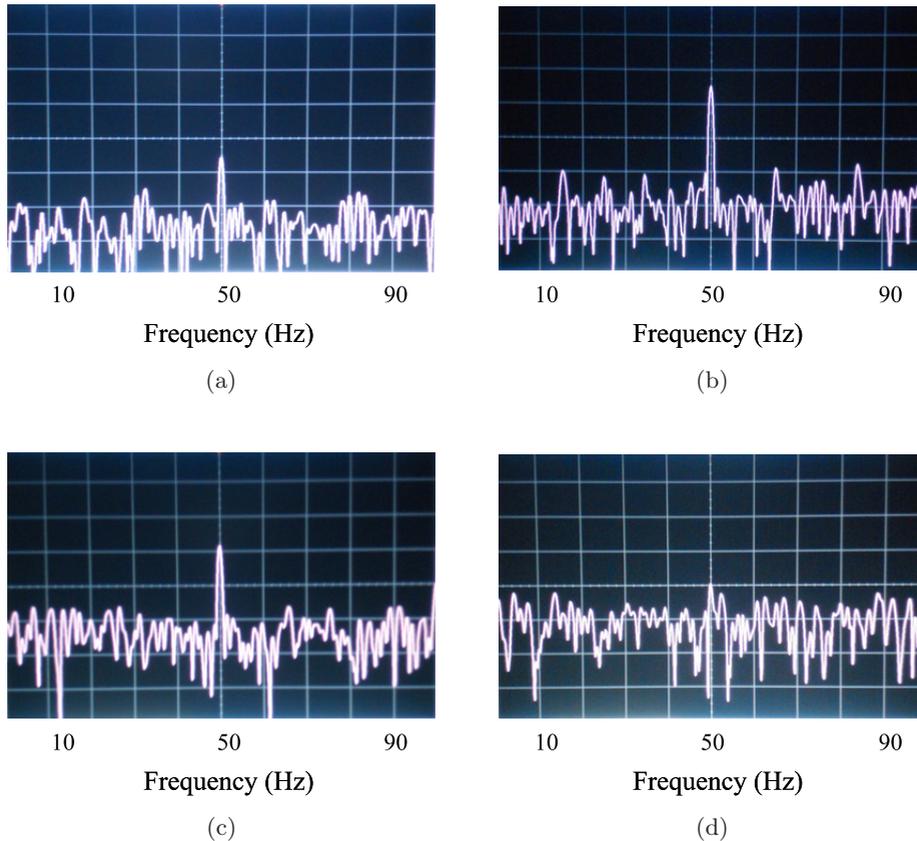


Fig. 2. The power spectrum of the voltage v_1 for four values of g . (a) $g = 1$ V, (b) $g = 1.3$ V, (c) $g = 1.55$ V and (d) $g = 2$ V. The values of other circuit parameters are $C_1 = 10$ nF, $C_2 = 100$ nF, $L = 18$ mH, $R = 1.98$ k Ω , $A = 0.3$ V, $\omega = 50$ Hz and $\Omega = 500$ Hz.

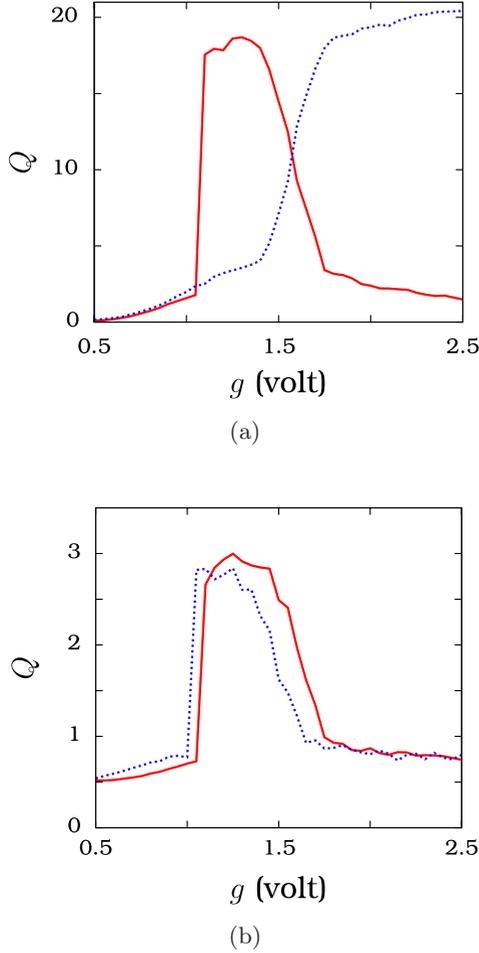


Fig. 3. (a) Response amplitudes Q at the low-frequency ω (continuous curve) and high-frequency Ω (dotted curve) associated with v_1 versus the control parameter g and (b) Q at the low-frequency ω associated with v_2 (continuous curve) and i_L (dotted curve) versus g .

at ω and Ω with g . As g increases from a small value, Q at ω increases slowly, varies sharply over an interval and reaches a maximum value at a critical value of g denoted as g_{VR} . The value of g_{VR} is found as 1.3 V. When g is increased further from g_{VR} the response amplitude decreases rapidly to a small value. This type of resonance behavior is not observed with Q at Ω . In Fig. 3(b) we plot Q of v_2 and i_L at ω as a function of g . Both Q at v_2 and i_L display resonance. In the rest of the analysis on the single Chua's circuit we consider Q of v_1 at ω .

Next, we illustrate the mechanism of vibrational resonance using a time series plot. Figure 4 presents $v_1(t)$ versus t for six fixed values of g . In the absence of a biharmonic force, the Chua circuit for the chosen parametric values has two stable equilibrium points $X_+ = (v_1, v_2, i_L) = (5.656 \text{ V}, 0 \text{ V},$

$-2.855 \text{ mA})$ and $X_- = (-5.656 \text{ V}, 0 \text{ V}, 2.855 \text{ mA})$ and one unstable equilibrium point $X_0 = (0, 0, 0)$. For $g = 0 \text{ V}$, $f = 0.3 \text{ V}$ and $\omega = 50 \text{ Hz}$, two period- T ($= 1/\omega$) orbits coexist — one orbit about X_+ and another about X_- . That is, on either side of $v_1 = 0$. When the system is driven further by the high-frequency force with $\Omega = 500 \text{ Hz}$ then for small

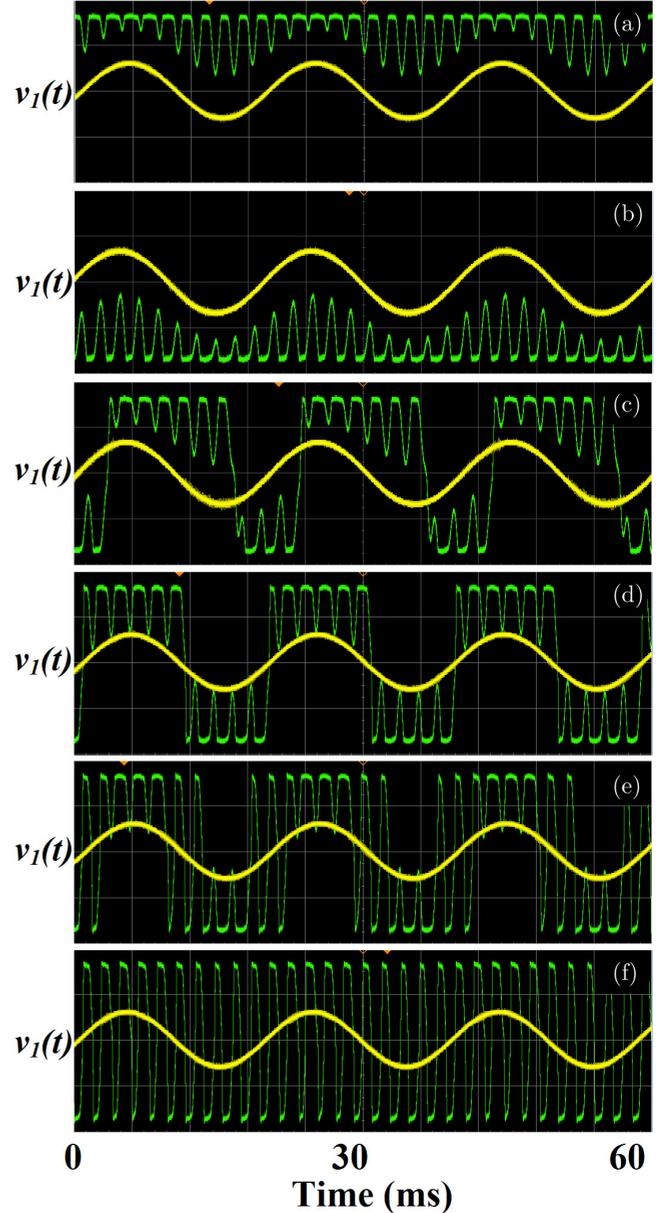


Fig. 4. Plot of $v_1(t)$ (green line) and the low-frequency periodic input signal $f \sin \omega t$ (yellow line) versus time t for five values of the amplitude g of the high-frequency periodic signal. (a) and (b) $g = 1 \text{ V}$, (c) $g = 1.15 \text{ V}$, (d) $g = 1.3 \text{ V}$, (e) $g = 1.55 \text{ V}$ and (f) $g = 2 \text{ V}$. In all the subplots the range of $v_1(t)$ is $[-10 \text{ V}, 10 \text{ V}]$. The low-frequency periodic input is 10 times enlarged in all the subplots for clarity.

values of g , the two periodic orbits coexist and $v_1(t)$ is modulated by the high-frequency force. This is shown in Figs. 4(a) and 4(b) for $g = 1$ V. At a certain value of g , crossing of $v_1 = 0$ takes place. We denote τ^+ as the time spent by the trajectory in the region $v_1 > 0$ before switching to the region $v_1 < 0$. Similarly, we define τ^- . τ^+ and τ^- are the residence times of the trajectory in the regions $v_1 > 0$ and $v_1 < 0$, respectively. We can then calculate the mean residence times τ_{MR}^+ and τ_{MR}^- . For g values just above the onset of switching between $v_1 < 0$ and $v_1 > 0$, the residence times τ_{MR}^+ and τ_{MR}^- are unequal. An example is shown in Fig. 4(c) where $g = 1.15$ V. τ_{MR}^+ and τ_{MR}^- vary with g . At the critical value $g = g_{VR} = 1.3$ V, $\tau_{MR}^+ = \tau_{MR}^- = T/2$ [see Fig. 4(d)]. There is a periodic switching between the regions $v_1 < 0$ and $v_1 > 0$ with period equal

to half the time of the period of the low-frequency input signal. The response amplitude Q is maximum at this value of g . This is the mechanism for vibrational resonance. Note that Q is not maximum, that is resonance does not occur, at the value of g for which the onset of crossing occurs. When g is further increased from g_{VR} the synchronization between $v_1(t)$ and the input signal $f \sin \omega t$ is lost [see Fig. 4(e)]. For sufficiently large values of g a rapid switching between the regions $v_1 < 0$ and $v_1 > 0$ occurs and now the oscillation is centered around the equilibrium point X_0 . This is evident in Fig. 4(f) where $g = 2$ V.

We experimentally analyze the influence of the parameters ω , f and Ω on resonance. Figure 5 presents the results. In Fig. 5(a) as Ω increases g_{VR} also increases but Q_{max} (the value of Q at

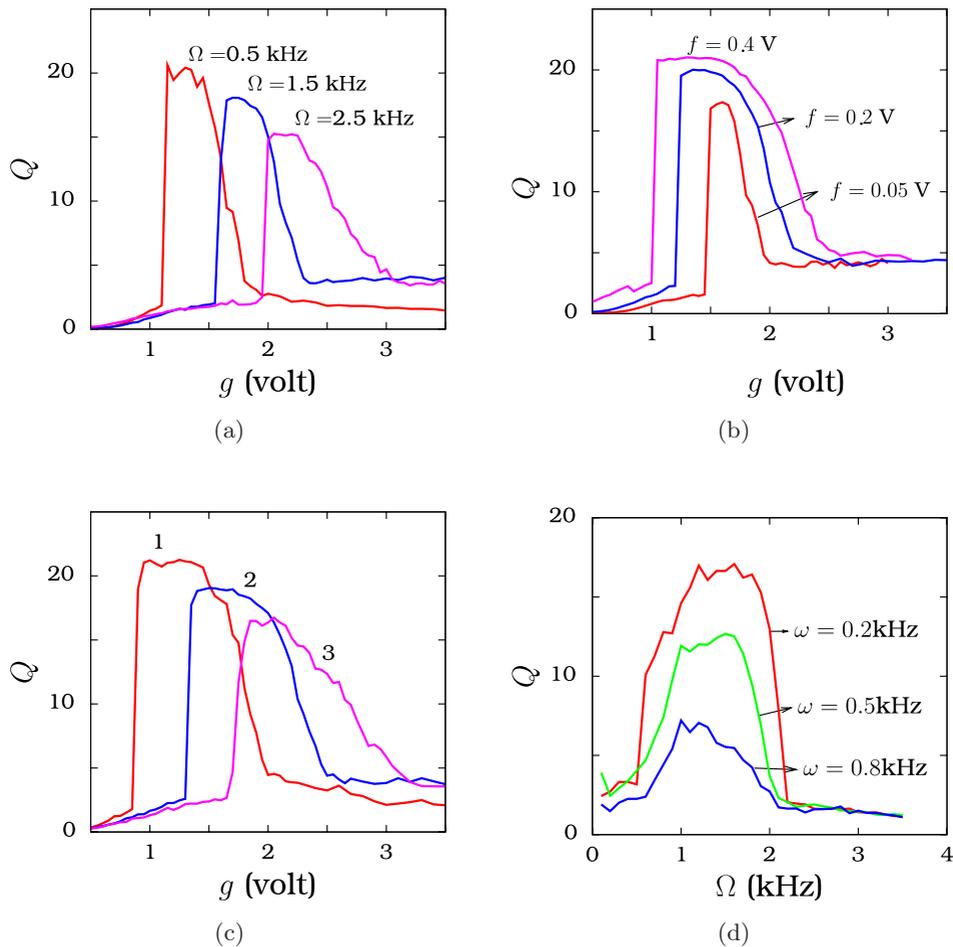


Fig. 5. The dependence of the response amplitude (Q) of the voltage v_1 versus the parameter g on (a) the high-frequency $\Omega = 0.5$ kHz, 1.5 kHz and 2.5 kHz with $f = 0.3$ V and $\omega = 50$ Hz, (b) the amplitude $f = 0.05$ V, 0.2 V and 0.4 V with $\omega = 50$ Hz and $\Omega = 1000$ Hz, (c) different combinations of ω and Ω with $\Omega/\omega = 10$ where for the curves 1, 2 and 3 the values of (ω, Ω) are $(50$ Hz, 500 Hz), $(150$ Hz, 1500 Hz) and $(250$ Hz, 2500 Hz) while $f = 0.5$ V and (d) variation of Q with the parameter Ω for three fixed values of ω with $f = 0.3$ V and $g = 1.75$ V.

resonance) decreases. The width of the bell shape part of the resonance profile increases when Ω increases. In Fig. 5(b), g_{VR} decreases while Q_{max} increases with an increase in f . The width of the bell shape part increases for increasing values of f . Figure 5(c) shows Q versus g for different set of values (ω, Ω) keeping the ratio Ω/ω as 10. Increase in ω and Ω leads to the effect observed in Fig. 5(a). In Fig. 5(d) increase in ω increases the value of Ω_{VR} but decreases the corresponding Q_{max} . Furthermore, we experimentally measure g_{VR} and Q_{max} for a range of values of high-frequency Ω for three different values of ω . Figure 6 depicts the variation of g_{VR} and Q_{max} with Ω . For all the fixed values of ω , g_{VR} increases while Q_{max} decreases almost linearly with Ω .

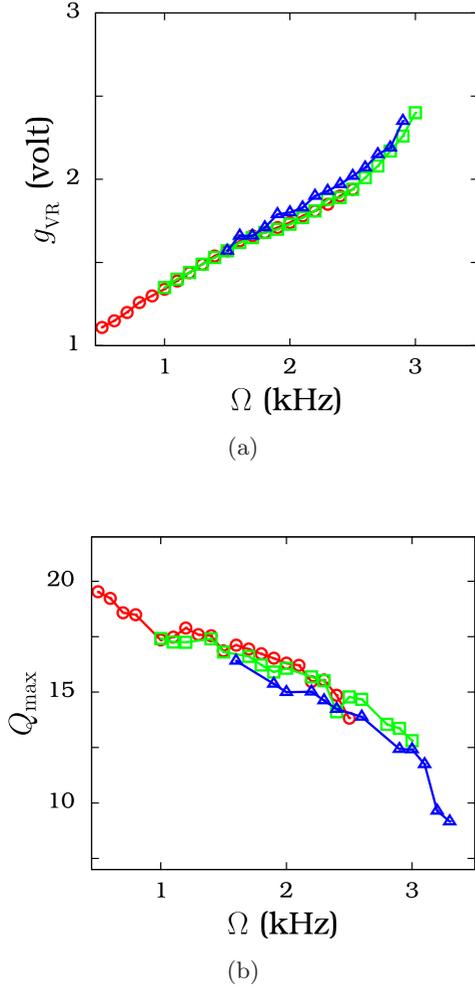


Fig. 6. Plot of (a) g_{VR} , the critical value of g at which resonance occurs and (b) Q_{max} , the value of Q at $g = g_{VR}$ versus the high-frequency Ω of the driving force. The values of the parameters are $f = 0.3$ V and $\omega = 50$ Hz (for the symbol circle), $\omega = 100$ Hz (square) and $\omega = 150$ Hz (triangle).

3. System of n -Coupled Chua's Circuits

In the previous section our focus is on the single Chua's circuit. The present section is devoted to the case of a system of n -coupled Chua's circuits with specific emphasis on signal propagation in the presence of a biharmonic external force. Study of coupled nonlinear systems are of great interest in different fields. It has been shown that the response of a nonlinear system can be improved by coupling it into an array of systems. Among the various types of coupling, the simple one is the unidirectional linear coupling introduced by Visarath In and his collaborators to induce oscillations in undriven, overdamped and bistable systems [In *et al.*, 2003a; In *et al.*, 2003b]. This coupling is found to give rise to synchronization [In *et al.*, 2005], propagation of waves of dislocations [Lindner & Bulsara, 2006], enhanced signal propagation in coupled overdamped bistable oscillators [Yao & Zhan, 2010] and in coupled maps [Rajasekar *et al.*, 2012] and propagation and annihilation of solitons [Lindner & Bulsara, 2006; Breen *et al.*, 2011]. Further, it is utilized in electronic sensors and microelectronic circuits [Razavi, 2008]. We consider a system of unidirectionally coupled n -Chua's circuits where only the first circuit is driven by the biharmonic force. We perform a PSpice simulation with $n = 75$ units. We show the evidence for improved transmission of low-frequency signal by the combined action of a high-frequency signal and a unidirectional coupling.

The system of n -coupled Chua's circuits is shown in Fig. 7. The coupling between the i th and $(i + 1)$ th circuits is made by feeding the voltage across the capacitor C_1 of the i th circuit to the $(i + 1)$ th circuit through a buffer as shown in Fig. 7. The state equations for the coupled circuits shown in Fig. 7 are [Kapitaniak *et al.*, 1994]

$$C_1 \frac{dv_1^{(i)}}{dt} = \left(\frac{1}{R} \right) (v_2^{(i)} - v_1^{(i)}) - f(v_1^{(i)}), \quad (3a)$$

$$C_2 \frac{dv_2^{(i)}}{dt} = \left(\frac{1}{R} \right) (v_1^{(i)} - v_2^{(i)} + i_L^{(i)}), \quad (3b)$$

$$L \frac{di_L^{(i)}}{dt} = -v_2^{(i)} + \delta_i (f \sin \omega t + g \sin \Omega t) + \epsilon_i (v_1^{(i-1)} - v_R), \quad (3c)$$

where, $\delta_1 = 1$, $\epsilon_1 = 0$ and $\delta_i = 0$ and $\epsilon_i = 1$ for $i = 2, 3, \dots, n$ and $v_R = i_L^{(i)} R C$.

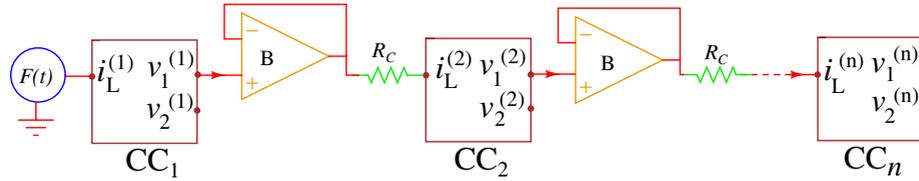


Fig. 7. The block diagram of a system of n unidirectionally coupled Chua's circuits. In the first circuit (CC_1), a biharmonic signal $F(t)$ is connected in series with current ($i_L^{(1)}$) and the remaining circuits are driven by the voltage v_1 of the previous circuit. Here B represents a buffer circuit and the arrowhead represents the direction of coupling.

The buffer circuit makes the coupling as unidirectional. We note that coupled circuits do not form a ring since the output of the last circuit is not fed to the first circuit. The system is a one-way open coupled Chua's circuits. The high input and low output impedances of the buffer ensures that the flow of the signal between i th and $(i + 1)$ th circuits is in forward direction, that is, from the i th circuit to the $(i + 1)$ th circuit only. The strength of the coupling is characterized by the coupling resistor R_C . Ullner *et al.* [2003] reported propagation of the low-frequency signal in a system of coupled oscillators. They considered excitable oscillators with all the oscillators driven by the high-frequency periodic force. First 100 oscillators alone are driven by the low-frequency force and are uncoupled. The rest of the oscillators are unidirectionally coupled. They performed numerical simulation. In our experimental work, we consider a simple setting of n -coupled circuits. As shown in Fig. 7, the first circuit alone is subject to biharmonic input signal and the coupling is unidirectional. In the systems considered in [Ullner *et al.*, 2003], if the coupling is removed then each oscillator exhibits oscillatory motion. In contrast to this, in the present case, if the coupling is removed then the first circuit alone exhibits oscillatory motion while the trajectory of all other circuits settle to the stable equilibrium point X_+ or X_- depending upon the initial state of the circuit.

We fix the values of the circuit parameters as $C_1 = 10$ nF, $C_2 = 100$ nF, $L = 18$ mH, $R = 2.15$ k Ω , $\omega = 100$ Hz, $\Omega = 1$ kHz and $f = 0.3$ V and treat R_C and g as the control parameters. Figure 8(a) presents the variation of Q_i with i (the number of the Chua circuit) for few values of g where $R_C = 1$ k Ω . For each fixed value of g , Q_i varies with i and approaches a limiting value. When $Q_2 > Q_1 (< Q_1)$ then Q_i increases (decreases) with i and reaches a saturation with $Q_{75} > Q_1 (< Q_1)$. The signal propagation through the coupled circuits is termed as undamped when $Q_{75} > Q_1$ is otherwise damped.

We measure Q_i for $g = 1.2$ V and for five different values of R_C . The result is presented in Fig. 8(b).

Figure 9 shows Q_i versus g and i for two values of the coupling resistor. For $R_C = 2.165$ k Ω , Q_i versus g [Fig. 9(a)] decays to zero as i increases. This is an example of damped signal propagation. In Fig. 9(b) where $R_C = 1$ k Ω the signal propagation

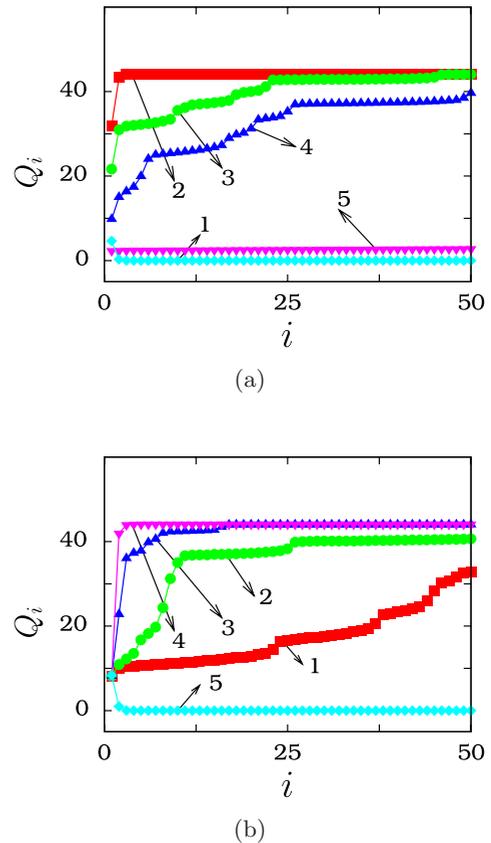


Fig. 8. (a) Q_i versus i (the number of the Chua circuit) for five values of g with $R_C = 1.0$ k Ω . For the curves 1–5 the values of g are 0.6 V, 0.85 V, 1.1 V, 1.15 V and 1.6 V. The values of the other parameters are set as $C_1 = 10$ nF, $C_2 = 100$ nF, $L = 18$ mH, $R = 2.15$ k Ω , $\omega = 100$ Hz, $\Omega = 1000$ Hz and $f = 0.3$ V and (b) Q_i versus i for five values of R_C with $g = 1.2$ V. The values of R_C for the curves 1–5 are 1 k Ω , 1.2 k Ω , 1.4 k Ω , 1.8 k Ω and 2 k Ω .

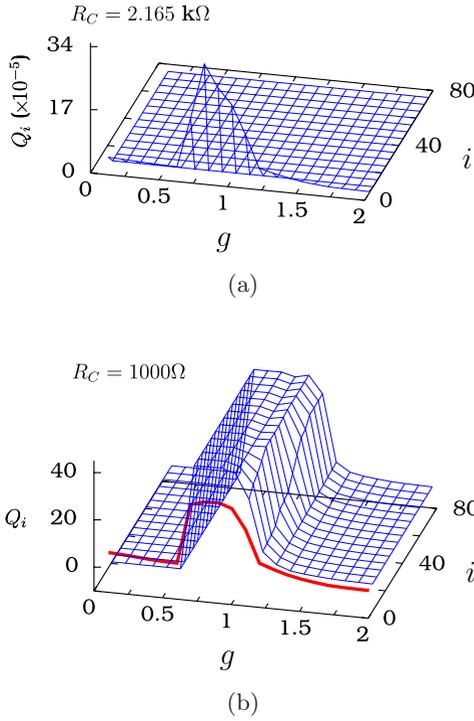


Fig. 9. Q_i as a function of i and g for two values of R_C illustrating (a) damped propagation of signal (for $R_C = 2.165 \text{ k}\Omega$) and (b) undamped signal propagation (for $R_C = 1 \text{ k}\Omega$) through the unidirectionally coupled Chua's circuits. The thick red curve in (b) represents Q_1 . In (a) Q_1 is not shown because Q_i 's with $i > 1$ are much lower than Q_1 .

is undamped $Q_i > Q_1, i > 1$ for a range of values of g . For $R_C \in [1 \text{ k}\Omega, 2.5 \text{ k}\Omega]$ and $g \in [0.5 \text{ V}, 2.0 \text{ V}]$ we experimentally identify the regions for which undamped signal propagation occurs. Figure 10 displays the result. Only for certain sets of values of R_C and g undamped signal propagation occurs. $Q_{75} = 0$ for (i) all values of R_C if $g < 0.68 \text{ V}$ and (ii) all

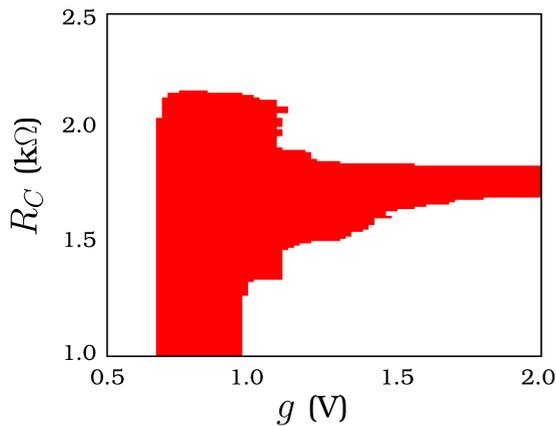


Fig. 10. Undamped signal propagation (marked by red color) in the $(g-R_C)$ parameters space.

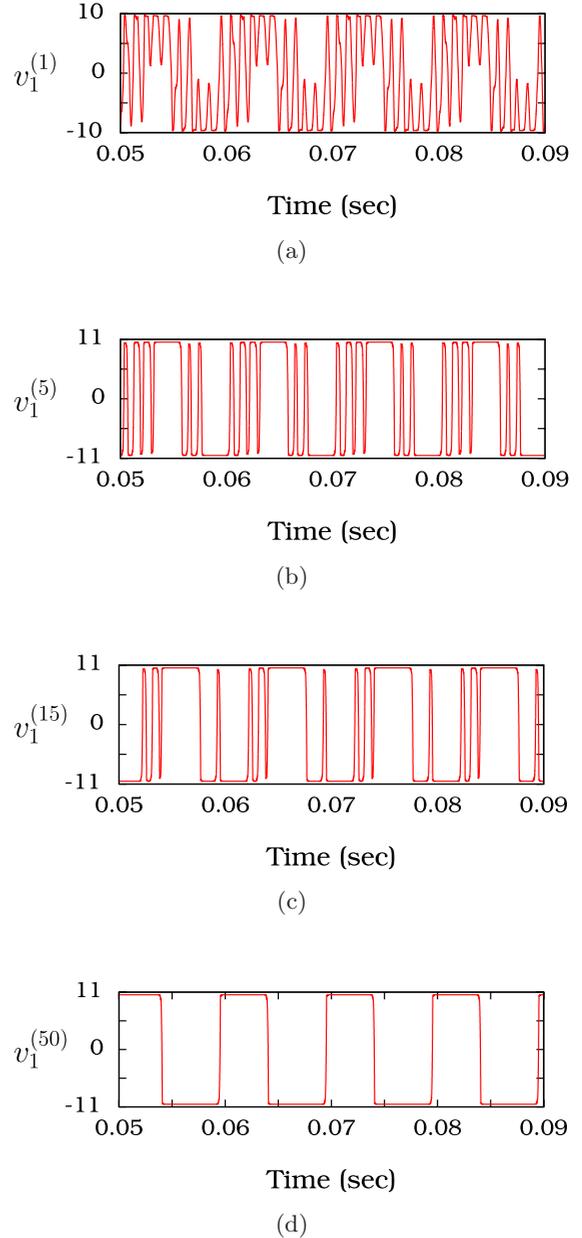


Fig. 11. Evolution of $v_1^{(i)}$ with time at four different nodes denoted as i where $R = 2.15 \text{ k}\Omega$, $R_C = 1 \text{ k}\Omega$ and $g = 1.1 \text{ V}$. Notice the suppression of high-frequency oscillations as i increases. (a) $i = 1$, (b) $i = 5$, (c) $i = 15$ and (d) $i = 50$.

values of g if $R_C \geq 2.165 \text{ k}\Omega$. Figure 11 presents another interesting result. In this figure we have plotted v_1 of the i th circuit versus t for four values of i . v_1 is periodic with period $T = 1/\omega$. The v_1 of the first circuit ($i = 1$) is modulated by the high-frequency drive. Since $\Omega/\omega = 10$, v_1 has ten peaks over one period. The high-frequency oscillation weakens as the number of circuit i increases as seen clearly in Figs. 11(b) and 11(c) for $i = 5$

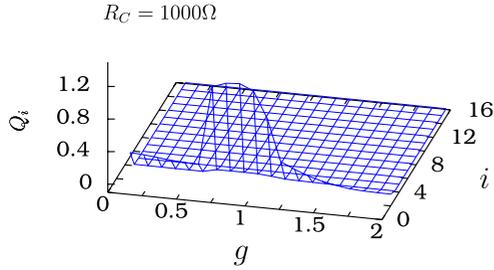


Fig. 12. Q_i as a function of g and i for $R_C = 1000\Omega$. For clarity Q_1 is not shown because $Q_1(g)$ is $\gg Q_i$ for $i = 2, 3, \dots$

and $i = 15$ respectively. For sufficiently large i the amplitude modulation of v_1 disappears. Moreover, the output signal appears as a rectangular pulse [Fig. 11(d)], of low-frequency ω . We wish to emphasize that in the coupled Chua’s circuits the biharmonic input signal is applied only to the first circuit. Essentially, the unidirectional coupling serves as a low-pass filter by weakening the propagation of the high-frequency component while enhancing the low-frequency component for a range of values g and R_C of the circuits.

Finally, we consider the n -coupled Chua’s circuit system with bidirectional coupling. In this case, the output of the i th circuit is fed as an input to the $(i + 1)$ th circuit and that of the circuit $(i + 1)$ is fed as an input to the i th circuit. The strength of the coupling is characterized by the coupling resistor R_C . We keep the values of the circuit parameters as chosen for unidirectional coupling and treat R_C and g as the control parameters. Figure 12 presents the variation of response amplitude Q_i with g and i for $R_C = 1000\Omega$. It clearly shows that the signal propagation is damped over the chain. We identified the nature of signal propagation for a wide range of values of g and R_C . Undamped signal propagation observed in the unidirectionally coupled circuits is not observed in the bidirectionally coupled circuits.

4. Conclusion

In the present work, we have considered one of the most widely investigated nonlinear circuits, namely Chua’s circuit which is capable of displaying a variety of complex dynamics. Here, we have shown that Chua’s circuit can also be used for weak signal detection and amplification through the vibrational resonance phenomenon. Resonance occurs when the output signal switches between two stable equilibrium states periodically with a period $T/2$ where T is the period of the low-frequency input signal.

The PSpice simulation study of a system of n -coupled Chua’s circuits reveals undamped signal propagation for a range of values of the amplitude g of the high-frequency input signal and the coupling parameter R_C . Another interesting result is the suppression of the high-frequency component in distant circuits while maintaining an enhanced signal propagation of low-frequency signal. The Q_i either decays to zero or approaches a nonzero constant values with increase in i . For most of the parametric choices considered in the present work, Q_i attained a stationary value for $i > 50$. Therefore, we have considered 75 coupled circuits. Study of stochastic, coherence and vibrational resonances in variants of Chua’s circuits such as switch controlled Chua’s circuit and multiscroll Chua’s circuit would bring out practical applications of these circuits in both weak signal detection (ac as well as dc) and output signal amplification.

A theoretical method has been developed to investigate vibrational resonance in nonlinear oscillators with polynomial potentials [Landa & McClintock, 2000; Blekhman & Landa, 2004; Chizhevsky, 2008]. In this approach one can obtain a linear system for the low-frequency component of the solution. Since, the equation of motion of Chua’s circuit is piecewise-linear it is very difficult to separately write the equations of motion for the slow and fast components (with frequencies ω and Ω , respectively).

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